

## Chapter 4 – Differential Relationship

- 4.1 Linear and Rotational Velocity
- 4.2 Motion of the Links of a Robot
- 4.3  $dx = Jdq$
- 4.4  $\Delta$  and  ${}^T\Delta$
- 4.5 Manipulator Jacobian
- 4.6 Inverse Jacobian
- 4.7 Singularity

## 4.1 Linear and Rotational Velocity

- Analyze the relationship of

$$dx = Jdq$$

$$J^{-1}dx = dq$$

- Linear velocity:

- Let  $Q$  be a vector, to specify its linear velocity, we need to select the reference frame. If a frame  $\{B\}$  is chosen, then:

$$\frac{d{}^B Q}{dt} = \lim_{\Delta t \rightarrow 0} \frac{{}^B Q(t + \Delta t) - {}^B Q(t)}{\Delta t} = {}^B V_Q$$

- When expressed in the frame  $\{A\}$ , then:

$${}^A ({}^B V_Q) = \frac{d{}^A Q}{dt} = {}^A R^B V_Q$$

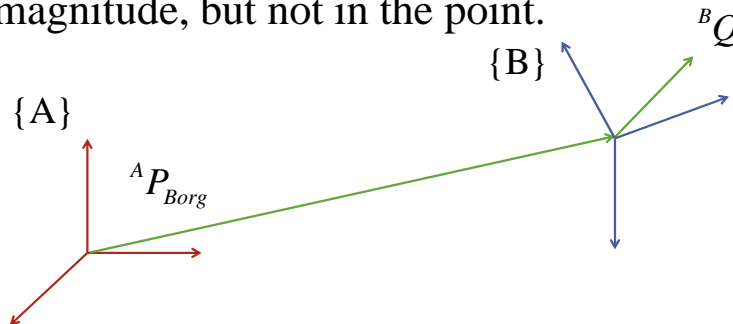
- Where  ${}^A R^B$  is the transformation from  $\{A\}$  to  $\{B\}$

## 4.1 Linear and Rotational Velocity

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- Note: that  ${}^B V_Q$  is significant only in direction and magnitude, but not in the point.



- Consider the movement of the origin of frame {B}

$${}^A V_Q = {}^A V_{Borg} + {}^A R^B V_Q$$

## 4.1 Linear and Rotational Velocity

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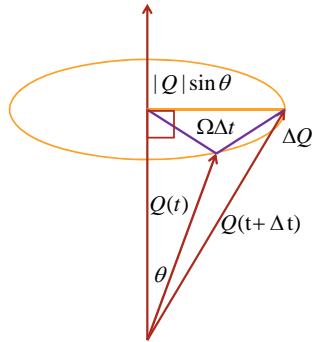
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- Rotational velocity:
  - Describe the rotational motion of a frame. Let  ${}^A \Omega_B$  denote the rotation of frame {B} relative to {A}.  ${}^A \Omega_B$  can be expressed in terms of different coordinates frames.
  - The question: How does a vector change with time as viewed from {A} when it is fixed in {B} and the systems are rotating?
  - Now the orientation of frame {B} with respect to frame {A} is changing in time, let the rotational velocity of {B} related to {A} is described by a vector called  ${}^A \Omega_B$  when  ${}^B Q$  is fixed in {B} and viewed from frame {B} ( ${}^B V_Q = 0$ ). However Q will have a velocity viewed from {A} due to  ${}^A \Omega_B$ .

## 4.1 Linear and Rotational Velocity

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$$|\Delta Q| = \left( {}^A Q \sin \theta \right) \left( {}^A \Omega_B \Delta t \right)$$

$${}^A V_Q = {}^A \Omega_B \times {}^A Q$$

$$|v| = |r\omega|$$

Q may be changing with respect to frame {B}

$${}^A V_Q = {}^A ({}^B V_Q) + {}^A \Omega_B \times {}^A Q$$

$$= {}^A R_B {}^B V_Q + {}^A \Omega_B \times ({}^A R_B {}^B Q)$$

Both linear and rotational

$${}^A V_Q = {}^A V_{Borg} + {}^A R_B {}^B V_Q + {}^A \Omega_B \times ({}^A R_B {}^B Q) - (*)$$

## 4.2 Motion of the Links of a Robot

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- Angular velocity of link  $i + 1$  with respect to coordinate of link  $i$  is about the  $Z_i$  axis ( $\theta_i + 1$ )

$$W_s = \begin{cases} \vec{Z}_i \dot{q}_{i+1} & \text{If link } i+1 \text{ is rotational} \\ 0 & \text{If link } i+1 \text{ is translational} \end{cases}$$

$$W_{i+1} = W_i + W_s = \begin{cases} W_i + \vec{Z}_i \dot{q}_{i+1} & \text{If link } i+1 \text{ is rotational} \\ W_i & \text{If link } i+1 \text{ is translational} \end{cases}$$

- Linear velocity

- Define:  $P_{i+1}^* = P_{i+1} - P_i$

$$V_{i+1} = \begin{cases} W_s \times P_{i+1}^* + W_i \times P_{i+1}^* + V_i, & i+1, R \\ \vec{Z}_i \cdot \dot{q}_{i+1} + W_i \times P_{i+1}^* + V_i, & i+1, P \end{cases}$$

$$= \begin{cases} W_{i+1} \times P_{i+1}^* + V_i, & i+1, R \\ \vec{Z}_i \cdot \dot{q}_{i+1} + W_{i+1} \times P_{i+1}^* + V_i, & i+1, P \end{cases}$$

## 4.3 $dx = Jdq$

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$$dX = \begin{bmatrix} dx \\ dy \\ dz \\ \delta x \\ \delta y \\ \delta z \end{bmatrix} \quad dq = \begin{bmatrix} d\theta_1 \\ d\theta_2 \\ \dots \\ \dots \\ \dots \\ d\theta_N \end{bmatrix}$$

$$X = f(q)$$

$$\frac{dX}{dt} = \frac{df(q)}{dt} = \frac{df(q)}{dq} \times \frac{dq}{dt}$$

$$\dot{X} = J * \dot{q} \quad POS = BASE * T_N * TOOL$$

## 4.3 $dx = Jdq$

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### □ Differential, Translation and Rotation

- ① With respect to base:

$$T + dT = Trans(dx, dy, dz) * Rot(k, d\theta) * T$$

$$dT = [Trans(dx, dy, dz) * Rot(k, d\theta) - I] * T = \Delta * T$$

For  $Rot(k, d\theta)$

$$\text{When } d\theta \rightarrow 0 \quad \begin{cases} \cos d\theta \approx 1 \\ \sin d\theta \approx d\theta \\ Vers(d\theta) \approx 0 \end{cases}$$

## 4.3 $dx = Jdq$

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$$Rot(k, d\theta) = \begin{pmatrix} 1 & -k_z d\theta & k_y d\theta & 0 \\ k_z d\theta & 1 & -k_x d\theta & 0 \\ -k_y d\theta & k_x d\theta & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$\Delta = \begin{pmatrix} 1 & 0 & 0 & dx \\ 0 & 1 & 0 & dy \\ 0 & 0 & 1 & dz \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & -k_z d\theta & k_y d\theta & 0 \\ k_z d\theta & 1 & -k_x d\theta & 0 \\ -k_y d\theta & k_x d\theta & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$\Delta = \begin{pmatrix} 0 & -k_z d\theta & k_y d\theta & dx \\ k_z d\theta & 0 & -k_x d\theta & dy \\ -k_y d\theta & k_x d\theta & 0 & dz \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

## 4.3 $dx = Jdq$

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② With respect to T

$$T + dT = T * Trans(dx, dy, dz) * Rot(k, d\theta)$$

$$dT = T * [Trans(dx, dy, dz) * Rot(k, d\theta) - I] = T * {}^T \Delta$$

$Rot(k, d\theta)$  can also be formulated as differential rotations  $\delta_x, \delta_y, \delta_z$  around x, y, z axes

$$Rot(x, \delta x) \cong \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & -\delta x & 0 \\ 0 & \delta x & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}, \quad Rot(y, \delta y) \cong \begin{pmatrix} 1 & 0 & \delta y & 0 \\ 0 & 1 & 0 & 0 \\ -\delta y & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}, \quad Rot(z, \delta z) \cong \begin{pmatrix} 1 & -\delta z & 0 & 0 \\ \delta z & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$Rot(x, \delta x) * Rot(y, \delta y) * Rot(z, \delta z) = \begin{pmatrix} 1 & -\delta z & \delta y & 0 \\ \delta z & 1 & -\delta x & 0 \\ -\delta y & \delta x & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

## 4.3 $dx = Jdq$

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$${}^T \Delta = \begin{pmatrix} 0 & -\delta z & \delta y & dx \\ \delta z & 0 & -\delta x & dy \\ -\delta y & \delta x & 0 & dz \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

$$\begin{cases} \delta x = k_x d\theta \\ \delta y = k_y d\theta \\ \delta z = k_z d\theta \end{cases}$$

## 4.4 $\Delta$ and ${}^T \Delta$

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$$dT = \Delta * T = T * {}^T \Delta$$

$${}^T \Delta = T^{-1} * \Delta * T$$

$$= \begin{pmatrix} n \cdot (\delta \times n) & n \cdot (\delta \times o) & n \cdot (\delta \times a) & n \cdot [(\delta \times P) + d] \\ o \cdot (\delta \times n) & o \cdot (\delta \times o) & o \cdot (\delta \times a) & o \cdot [(\delta \times P) + d] \\ a \cdot (\delta \times n) & a \cdot (\delta \times o) & a \cdot (\delta \times a) & a \cdot [(\delta \times P) + d] \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$\text{From } a \cdot (b \times c) = -b \cdot (a \times c) = b \cdot (c \times a)$$

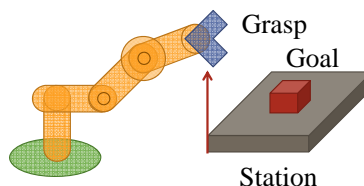
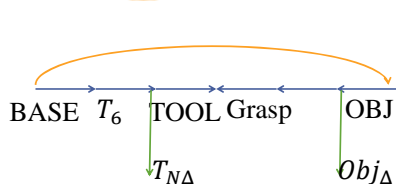
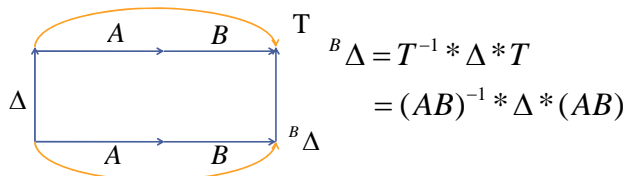
$$\Rightarrow \begin{pmatrix} 0 & -\delta \cdot a & \delta \cdot o & (\delta \times P) \cdot n + d \cdot n \\ \delta \cdot a & 0 & -\delta \cdot n & (\delta \times P) \cdot o + d \cdot o \\ -\delta \cdot o & \delta \cdot n & 0 & (\delta \times P) \cdot a + d \cdot a \\ 0 & 0 & 0 & 1 \end{pmatrix}, T_d = \begin{pmatrix} (\delta \times P + d) \cdot n \\ (\delta \times P + d) \cdot o \\ (\delta \times P + d) \cdot a \end{pmatrix}, T_\delta = \begin{pmatrix} \delta \cdot n \\ \delta \cdot o \\ \delta \cdot a \end{pmatrix}$$

## 4.4 $\Delta$ and $T \Delta$

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□ Assume  $T=A*B$



Know  ${}^{Obj} \Delta$  find  ${}^{T6} \Delta$

$$T = Grasp * TOOL^{-1}$$

$$T = OBJ^{-1} * BASE * T_6$$

$${}^{TN} \Delta = T^{-1} * {}^{Obj} \Delta * T$$

## 4.5 Manipulator Jacobian

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$$T_N = A_1 * A_2 * \dots * A_N$$

$$q_i = \begin{cases} \theta_i, & \text{revolute} \\ d_i, & \text{prismatic} \end{cases}$$

$$A_i = \begin{pmatrix} C\theta_i & -S\theta_i C\alpha_i & S\theta_i S\alpha_i & a_i C\theta_i \\ S\theta_i & C\theta_i C\alpha_i & -C\theta_i S\alpha_i & a_i S\theta_i \\ 0 & S\alpha_i & C\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

For revolute joint

$$\frac{dA_i}{d\theta_i} = \begin{pmatrix} -S\theta_i & -C\theta_i C\alpha_i & C\theta_i S\alpha_i & -a_i S\theta_i \\ C\theta_i & -S\theta_i C\alpha_i & S\theta_i S\alpha_i & a_i C\theta_i \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix} = \begin{pmatrix} 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix} A_i$$

## 4.5 Manipulator Jacobian

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For prismatic joint

$$\frac{dA_i}{dd_i} = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{pmatrix} \quad dA_i = {}^{i-1}\Delta_i A_i dq_i = A_i {}^i\Delta_{i+1} dq_i$$

$\uparrow \begin{pmatrix} {}^{i-1}d_i \\ {}^{i-1}\delta_i \end{pmatrix} \qquad \uparrow \begin{pmatrix} {}^i d_{i+1} \\ {}^i \delta_{i+1} \end{pmatrix}$

For revolute joint, only (rotational error) around  $Z_{i-1}$  axis

$${}^{i-1}d_i = 0, {}^{i-1}\delta_i = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

For prismatic joint, only (translational error) along  $Z_{i-1}$  axis

$${}^{i-1}\delta_i = 0, {}^{i-1}d_i = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

## 4.5 Manipulator Jacobian

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Due to errors in  $dA_i, i = 1, 2, \dots, N$

$$\begin{aligned} T_N + dT_N &= A_1 * A_2 * \dots * (A_i + dA_i) * \dots * A_N \\ &\quad \Downarrow \\ &= T_N + (A_1 * \dots * A_{i-1} * {}^{i-1}\Delta_i * A_i * A_{i+1} * \dots * A_N) dq_i \end{aligned}$$

$$\begin{aligned} dT_N &= \boxed{A_1 * \dots * A_N} * \boxed{[A_1 * \dots * A_N]^{-1} * {}^{i-1}\Delta_i * [A_1 * \dots * A_N]} * dq_i \\ &= \boxed{T_N} * \boxed{{}^N\Delta_i} * dq_i \end{aligned}$$

$$\begin{aligned} {}^N\Delta_i &= [A_1 * \dots * A_N]^{-1} * {}^{i-1}\Delta_i * [A_1 * \dots * A_N] \\ &= U_{i-1}^{-1} * {}^{i-1}\Delta_i * U_{i-1} \quad \text{Where } U_{i-1} = A_i * \dots * A_N \end{aligned}$$



## 4.5 Manipulator Jacobian

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For revolute joint

$${}^{i-1}d_i = 0, {}^{i-1}\delta_i = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

$${}^{T_N}d_i = \begin{pmatrix} n \cdot [({}^{i-1}\delta_i \times P) + {}^{i-1}d_i] \\ o \cdot [({}^{i-1}\delta_i \times P) + {}^{i-1}d_i] \\ a \cdot [({}^{i-1}\delta_i \times P) + {}^{i-1}d_i] \end{pmatrix} = \begin{pmatrix} P_x n_y - n_x P_y \\ P_x o_y - o_x P_y \\ P_x a_y - a_x P_y \end{pmatrix}$$

Where n, o, a, p are of  $U_{i-1}$

$${}^{T_N}\delta_i = \begin{pmatrix} n \cdot {}^{i-1}\delta_i \\ o \cdot {}^{i-1}\delta_i \\ a \cdot {}^{i-1}\delta_i \end{pmatrix} = \begin{pmatrix} n_z \\ o_z \\ a_z \end{pmatrix}$$

## 4.5 Manipulator Jacobian

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For prismatic joint

$${}^{i-1}d_i = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}, {}^{i-1}\delta_i = 0 \quad {}^{T_N}d_i = \begin{pmatrix} n_z \\ o_z \\ a_z \end{pmatrix}, {}^{T_N}\delta_i = 0$$

$$\text{In total } {}^{T_N}\Delta = \sum_{i=1}^N (U_{i-1}^{-1} * {}^{i-1}\Delta_i * U_{i-1})$$

$$\begin{bmatrix} {}^{T_N}d \\ {}^{T_N}\delta \end{bmatrix} = \begin{pmatrix} \vdots & \vdots & \vdots & \vdots \\ {}^{T_N}\Delta_1 & {}^{T_N}\Delta_2 & \cdots & {}^{T_N}\Delta_N \\ \vdots & \vdots & \vdots & \vdots \\ \vdots & \vdots & \vdots & \vdots \end{pmatrix} \begin{pmatrix} dq_1 \\ dq_2 \\ \vdots \end{pmatrix}$$

## 4.6 Inverse Jacobian

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- Using  $dq = J^{-1}dx$  to invert the J matrix directly is very inefficient. We need to consider the case when  $J^{-1}$  doesn't exist ( $\det J = 0$ , not full rank)

### ① R.Paul's method

- a) From  ${}^{T_6}d, {}^{T_6}\delta$  compute  $dT_6 = T_6 * {}^{T_6}\Delta$

$$= \begin{pmatrix} dn_6 & do_6 & da_6 & dp_6 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

## 4.6 Inverse Jacobian

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### b) Kinematic solution.

- Differentiate the solution given a value of  $T_6$ , the expressions for each differential changes are functions of  $dT_6$  and those  $d\theta$ 's that are already obtained.

#### ● Example: PUMA 560

- For  $\theta_1$

$$-S_1P_x + C_1P_y = d_3$$

$$(-C_1P_x - S_1P_y)d\theta_1 - (S_1dP_x - C_1dP_y) = 0$$

$$d\theta_1 = -\frac{S_1dP_x - C_1dP_y}{C_1P_x + S_1P_y}$$

- Similarly  $d\theta_2 \dots d\theta_6$  can be obtained

## 4.6 Inverse Jacobian

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- ② Method frequently used in the industries in the past
  - a) Compute  $dT_6$
  - b) Compute  $T_6^N = T_6 + dT_6 \Rightarrow T^T \Delta = \frac{\partial T \Delta}{\partial q} \partial q$
  - c) Compute new joint solution from  $T_6^N$
  - d)  $dq = q^N - q$
- ③ Neural Network Approach
- ④ Fuzzy Approach
- ⑤ “An efficient Solution of Differential Inverse Kinematics Problem for Wrist-Partitioned Robots” IEEE Trans. Rob. & Auto. Vol. 6(1) PP. 117-123, 1990

$$J^{wrist} = \begin{pmatrix} J_1 & 0 \\ J_2 & J_3 \end{pmatrix} \quad J^{-1} = [J_1]^{-1} [J_3]^{-1}$$

## 4.7 Singularity

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- $J = 0 \Rightarrow dq = J^{-1} dx$  can not be obtained
- 3 cases for PUNA560:
  - ① Links 2 and 3 are fully extended.
  - ② Joint 5 at its zero position.
  - ③ The end of link 3 aligns with the axis of robot trunk.

